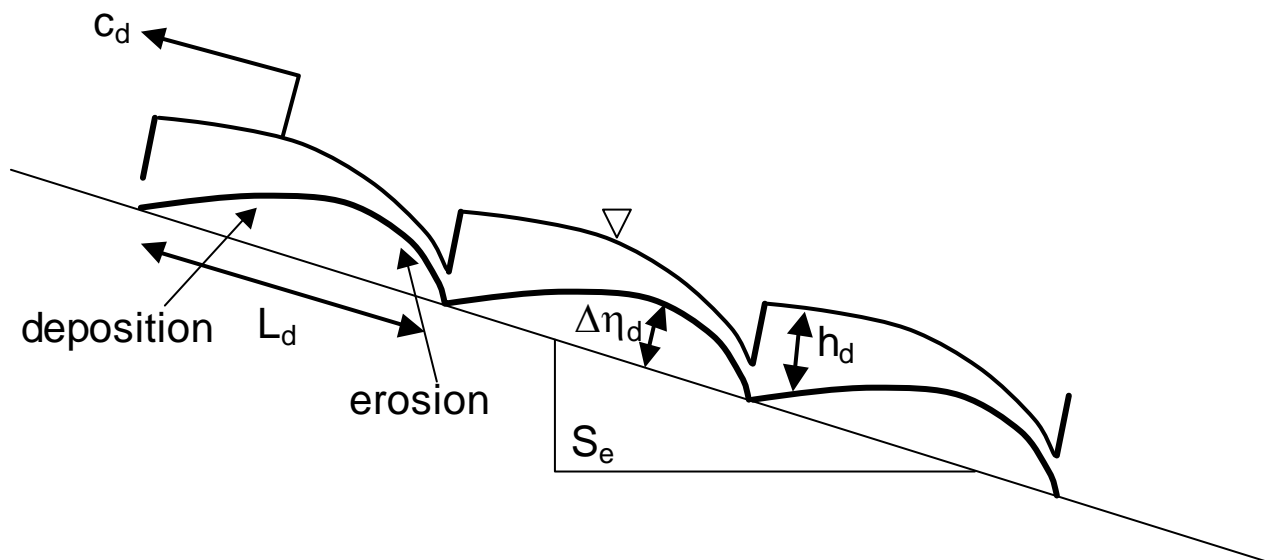


## CHAPTER 2 TRANSPORTATIONAL CYCLIC STEPS



(view slides)

### *Features*

- Dominant transport mode: suspended sediment
- Spatially periodic, or cyclic
- Each step bounded by hydraulic jump
- Froude-subcritical  $\rightarrow$  supercritical down step
- Deposition upstream, erosion downstream
- Migrates upstream with constant speed  $c_d$
- Steps maintain permanent form as they migrate

Question: is an equilibrium mobile-bed Froude-supercritical flow a *stable* equilibrium?

**St. Venant shallow water equations**  
**Exner Equation of sediment continuity**  
**Quasi-steady approximation**

$$u_d \frac{du_d}{dx_d} = -g \frac{dh_d}{dx_d} - g \frac{d\eta_d}{dx_d} - C_f u_d^2$$

$$u_d h_d = q_w$$

$$\frac{d}{dx_d} (q_w \chi_d) = v_s (E - r_o \chi_d)$$

$$(1 - \lambda_p) \frac{\partial \eta_d}{\partial t_d} = v_s (r_o \chi_d - E)$$

Here “d” denotes “dimensioned”

$x_d$  = long coordinate

$t_d$  = time

$h_d$  = depth

$\eta_d$  = bed elevation

$u_d$  = flow velocity

$g$  = grav. Accel.

$v_s$  = sed. fall velocity

$\lambda_p$  = bed porosity

$C_f$  = friction coefficient      $r_o = \chi_{db}/\chi_d, o(1)$

$q_w$  = water discharge/width (constant here)

$\chi_d$  = volume concentration of suspended sediment (dimensionless)

## “Constitutive” Relations

### *Resistance*

$C_f$  = specified constant

### *Entrainment into suspension*

$$E = \alpha_t [\tau_b^* - \tau_{th}^*]^n$$

$$\tau_b^* = \frac{\tau_b}{\rho R g D} \quad \tau_b = \rho C_f u_d^2$$

$$\alpha_t = \alpha_t(\mathbf{Re}_p) \quad \mathbf{Re}_p = \frac{\sqrt{R g D} D}{\nu}$$

$$\tau_{th}^* = \frac{C_f u_{dt}^2}{R g D}$$

$u_{dt}$  = threshold velocity for bed erosion

$D$  = grain size

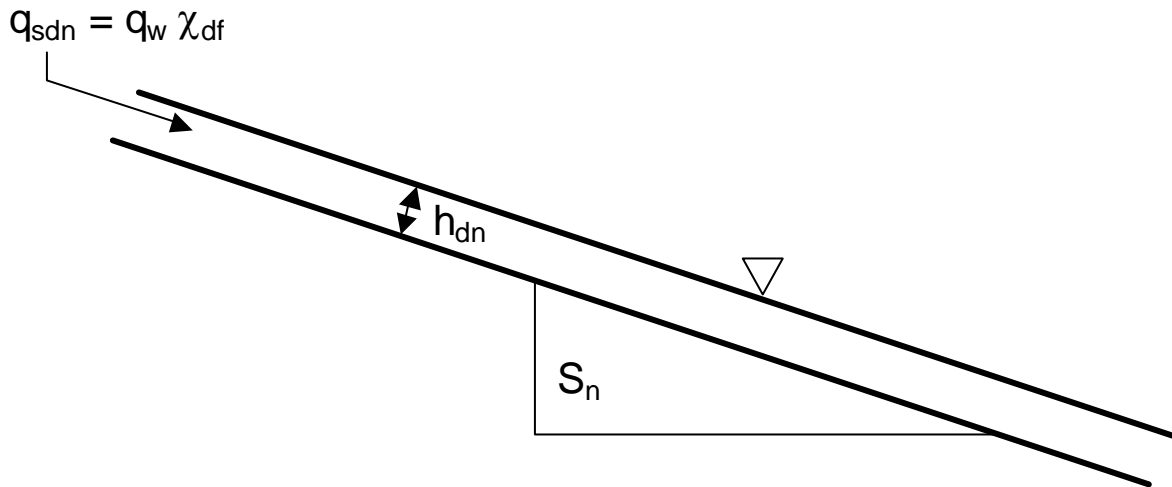
$\nu$  = kinematic viscosity of water

$$R = (\rho_s/\rho) - 1 \cong 1.65 \quad n \geq 1.5$$

After some work,

$$E = \alpha_t (\tau_{th}^*)^2 \left[ \left( \frac{u_d}{u_{dt}} \right)^2 - 1 \right]^n$$

## Equilibrium mobile-bed state without steps



$$q_w = \text{constant}$$

$$q_{sdn} = \text{feed sediment transport rate} = q_w \chi_{df} = \text{constant}$$

“n” = no steps

$$C_f u_{dn}^2 = g h_{dn} S_n$$

$$u_{dn} h_{dn} = q_w$$

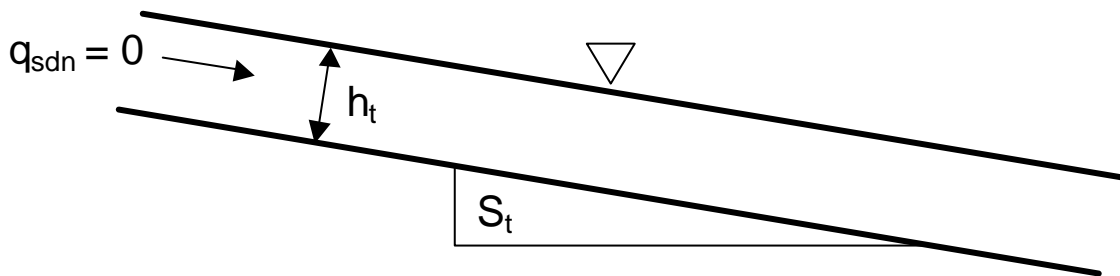
Assume thin flows, vigorous suspension  $\therefore r_o \cong 1$

$$\chi_{dn} = E_n = \chi_{df} \quad E_n = \alpha_t (\tau_{th}^*)^2 \left[ \left( \frac{u_{dn}}{u_{dt}} \right)^2 - 1 \right]^n$$

Specify  $q_w$ ,  $\chi_{df}$  ( $R$ ,  $d$ ,  $C_f$ , etc.): compute  $u_{dn}$ ,  $h_{dn}$ ,  $S_n$

$$C_f \mathbf{Fr}_n^2 = S_n \quad \mathbf{Fr}_n^2 = \frac{u_{dn}^3}{g q_w} > 1$$

## Equilibrium state at the threshold of bed erosion



$q_w$  = same as case of mobile-bed equilibrium

$q_{sdn} = \chi_{df} = 0$  (no sediment feed)

$$u_{dt} = \left( \frac{RgD\tau_{th}^*}{C_f} \right)^{1/2}$$

$$C_f u_{dt}^2 = gh_{dt} S_t$$

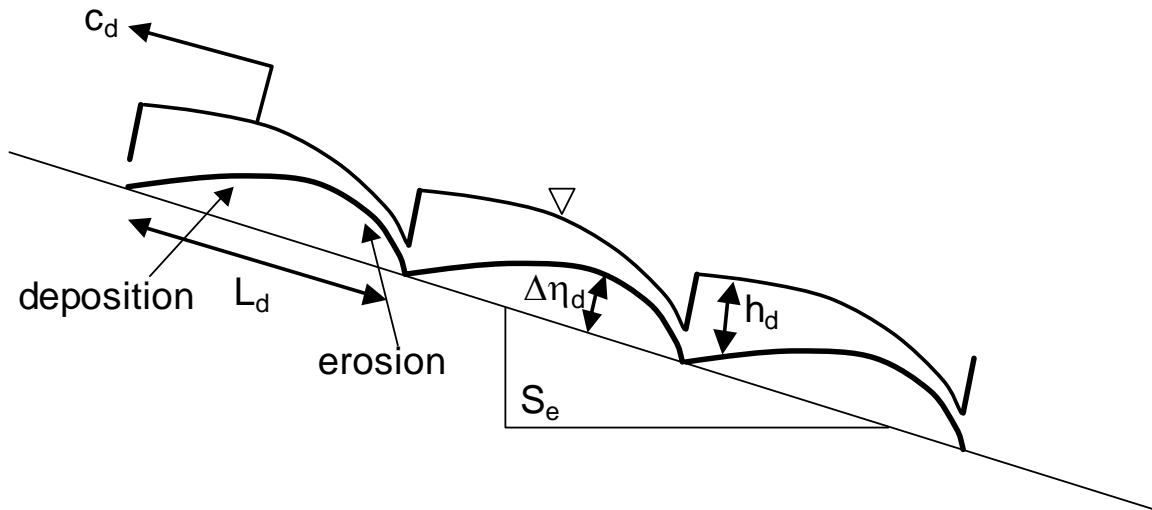
$$u_{dt} h_{dt} = q_w$$

Reduce to

$$C_f \mathbf{Fr}_t^2 = S_t \quad \mathbf{Fr}_t^2 = \frac{u_{dt}^3}{gq_w}$$

Here we assume  $\mathbf{Fr}_n > 1$ ,  $\mathbf{Fr}_t < 1$

## Cyclic steps of permanent form



$c_d$  = wave speed (positive upstream)

$L_d$  = wave length

$S_e$  = equilibrium average slope with steps

In general,

$$\eta_d = \eta_{do} - S_e x_d + \eta_{ed}(x_d, t_d)$$

$$u_d = u_d(x_d, t_d)$$

$$h_d = h_d(x_d, t_d)$$

$$\chi_d = \chi_d(x_d, t_d)$$

Transform to

$$\tilde{x}_d = x_d + c_d t_d \quad \tilde{t}_d = t_d$$

and drop dependency in  $\tilde{t}_d$

## Result:

Functional forms:

$$\begin{aligned}\eta_{ed} &= \eta_{ed}(\tilde{x}_d) & \mathbf{u}_d &= \mathbf{u}_d(\tilde{x}_d) \\ h_d &= h_d(\tilde{x}_d) & \chi_d &= \chi_d(\tilde{x}_d)\end{aligned}$$

St: Venant equations

$$\mathbf{u}_d \frac{d\mathbf{u}_d}{d\tilde{x}_d} = -g \frac{dh_d}{d\tilde{x}_d} + gS_e - g \frac{d\eta_{ed}}{d\tilde{x}_d} - C_f \mathbf{u}_d^2$$

$$\mathbf{u}_d h_d = q_w$$

$$q_w \frac{d\chi_d}{d\tilde{x}_d} = v_s (E - \chi_d)$$

Exner equation of bed sediment continuity

$$(1 - \lambda_p) c_d \frac{d\eta_{ed}}{d\tilde{x}_d} = -v_s (E - \chi_d)$$

## Boundary conditions

Bed elevation

$$\eta_{ed} \Big|_{\tilde{x}_d=0} = 0 \quad \eta_{ed} \Big|_{\tilde{x}_d=L_d} = 0$$

Flow velocity

$$\mathbf{u}_d \Big|_{\tilde{x}_d=0} = \mathbf{u}_{dt}$$

$$\mathbf{u}_d \Big|_{\tilde{x}_d=L_d} = \mathbf{u}_{dcon} \equiv \left( \frac{\sqrt{1 + 8\mathbf{Fr}_t^2} - 1}{2} \right)^{-1} \mathbf{u}_{dt}$$

Suspended sediment concentration

$$\frac{1}{T_d} \mathbf{q}_w \int_0^{T_d} \chi_d dt_d = \mathbf{q}_w \chi_{df} \quad T_d = \frac{L_d}{c_d}$$

or thus

$$\frac{1}{L_d} \int_0^{L_d} \chi_d d\tilde{x}_d = \chi_{df}$$



## Non-dimensionalization

Introduce

$$u_d = u_{dt} u \quad h_d = \frac{q_w}{u_{dt}} h \quad \eta_{ed} = \frac{q_w}{u_{dt}} \eta$$

$$\tilde{x}_d = \frac{q_w}{u_{dt}} \frac{1}{S_t} x \quad \chi_d = \chi_{df} \chi$$

Substitute into governing equations:

$$\frac{du}{dx} = \frac{S_r + \frac{\omega}{c}(E - \chi) - u^3}{\mathbf{Fr}_t^2 u - u^{-2}}$$

$$\frac{d\chi}{dx} = \omega(E - \chi)$$

$$c \frac{d\eta}{dx} = -\omega(E - \chi)$$

where

$$c = \frac{(1 - \lambda_p)}{u_t \chi_f} c_d \quad \omega = \frac{v_s}{S_t u_t} \quad L = S_t \frac{u_t}{q_w} L_d$$

$$S_r = S_e / S_t$$

## Non-dimensionalization continued

$$\frac{du}{dx} = \frac{S_r + \frac{\omega}{c}(E - \chi) - u^3}{\mathbf{Fr}_t^2 u - u^{-2}}$$

$$\frac{d\chi}{dx} = \omega(E - \chi)$$

$$c \frac{d\eta}{dx} = -\omega(E - \chi)$$

where

$$E = \frac{(u^2 - 1)^n}{(u_n^2 - 1)^n}$$

Boundary conditions

$$\eta|_{x=0} = 0 \quad \eta|_{x=L} = 0$$

$$u|_{x=0} = 1 \quad u|_{x=L} = \left( \frac{\sqrt{1 + 8\mathbf{Fr}_t^2} - 1}{2} \right)^{-1}$$

$$L = \int_0^L \chi dx$$

## Reduction

Between

$$\frac{d\chi}{dx} = \omega(E - \chi) \quad c \frac{d\eta}{dx} = -\omega(E - \chi)$$

find

$$\eta = \frac{1}{c}(\chi|_{x=0} - \chi)$$

Then apply

$$\eta|_{x=0} = 0 \quad \eta|_{x=L} = 0$$

To get

$$\chi|_{x=L} = \chi|_{x=0}$$

## Final form of the problem

$$\frac{du}{dx} = \frac{S_r + \frac{\omega}{c}(E - \chi) - u^3}{\mathbf{Fr}_t^2 u - u^{-2}}$$

$$\frac{d\chi}{dx} = \omega(E - \chi)$$

where

$$E = \frac{(u^2 - 1)^n}{\left[ \left( \frac{\mathbf{Fr}_n}{\mathbf{Fr}_t} \right)^{4/3} - 1 \right]^n}$$

and

$$u|_{x=0} = 1 \quad u|_{x=L} = \left( \frac{\sqrt{1 + 8\mathbf{Fr}_t^2} - 1}{2} \right)^{-1}$$

$$\chi|_{x=L} = \chi|_{x=0} \quad L = \int_0^L \chi dx$$

## Character of the problem

*Overspecified system of ordinary differential equations*

2 first-order differential equations in  $u, \chi$

+

4 parameters,  $\mathbf{Fr}_t, \mathbf{Fr}_n, S_r, c$

*subject to*

4 boundary conditions

Thus if any two of  $\mathbf{Fr}_t, \mathbf{Fr}_n, S_r, c$  are specified,  $u, \chi$  and the other two can be computed

But note the singularity in the denominator!

$$\frac{du}{dx} = \frac{S_r + \frac{\omega}{c}(E - \chi) - u^3}{\mathbf{Fr}_t^2 u - u^{-2}}$$

$$\mathbf{Fr}^2 = \frac{u_d^3}{gq_w} = \mathbf{Fr}_t^2 u^3$$

$$\therefore \mathbf{Fr} = 1 \text{ when } u = \mathbf{Fr}_t^{-2/3}$$

## Removal of singularity

Thus denominator is singular at  $x = x_1$  where

$$u = u_1 \equiv \mathbf{Fr}_t^{-2/3}$$

Thus numerator of right-hand side of

$$\frac{du}{dx} = \frac{S_r + \frac{\omega}{c}(E - \chi) - u^3}{\mathbf{Fr}_t^2 u - u^{-2}}$$

must also vanish, yielding the constraint

$$\chi_1 = \frac{(\mathbf{Fr}_t^{-4/3} - 1)^n}{\left[ \left( \frac{\mathbf{Fr}_n}{\mathbf{Fr}_t} \right)^{4/3} - 1 \right]^n} - \frac{c}{\omega} (\mathbf{Fr}_t^{-2} - S_r)$$

at  $x = x_1$

## Removal of singularity, continued

Now at  $x = x_1$

$$\frac{du}{dx} = \frac{0}{0}$$

Applying L'hospital's rule,

$$3\mathbf{Fr}_t^2 (u'_1)^2 + (3\mathbf{Fr}_t^{-4/3} - \frac{\omega}{c} E_{u1})u'_1 + \omega(\mathbf{Fr}_t^{-2} - S_r) = 0$$

where

$$u'_1 = \left. \frac{du}{dx} \right|_{x_1}$$

$$E_{u1} = \left. \frac{dE}{du} \right|_{x_1} = \frac{n\mathbf{Fr}_t^{-2/3} (\mathbf{Fr}_t^{-4/3} - 1)^{n-1}}{\left[ \left( \frac{\mathbf{Fr}_n}{\mathbf{Fr}_t} \right)^{4/3} - 1 \right]^n}$$

## Solution procedure

Specify all parameters such as  $\tau_{th}^*$ ,  $\omega$ ,  $C_f$ , etc.

Specify values of  $\mathbf{Fr}_n$  and  $\mathbf{Fr}_t$ .

Guess values of  $S_r$ ,  $c$

Define the variable  $x_r = x - x_1$ .

Integrate upstream from  $x_r = 0$  in  $u$  and  $\chi$  until

$$x_r = -L_u$$

where

$$u = 1 \quad (\text{threshold conditions})$$

Integrate downstream from  $x_r = 0$  in  $u$  and  $\chi$  until

$$x_r = L_d$$

where

$$u = \left( \frac{\sqrt{1 + 8\mathbf{Fr}_t^2} - 1}{2} \right)^{-1}$$

For each  $S_r$ ,  $c$  thus get

$$L = L_u + L_d = L(c, S_r)$$

$$u = u(x; c, S_r) \quad \chi = \chi(x; c, S_r)$$



## Solution procedure, continued

Write remaining two boundary conditions in the form

$$F_1(c, S_r) \equiv$$

$$\chi[L(c, S_r); c, S_r] - \chi(0; c, S_r) = 0$$

$$F_2(c, S_r) \equiv$$

$$L(c, S_r) - \int_0^{L(c, S_r)} \chi(x; c, S_r) dx = 0$$

Use bisection or Newton-Raphson technique to obtain improved guesses of  $c$  and  $S_r$  until convergence

Sample case:

Experiments using 19 micron, 45 micron and 120 micron silica flour

Depths are 1.1 to 7.0 mm

Flow before steps form almost always supercritical:  $\mathbf{Fr}_n > 1$